



# Formation kinetics and cation inversion in mechanically activated $\text{MgAl}_2\text{O}_4$ spinel ceramics

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## Abstract

Solid-state mechanical activation of MgO and  $\alpha\text{-Al}_2\text{O}_3$  powders was used to produce  $\text{MgAl}_2\text{O}_4$ . The cation site occupancy in the resulting  $\text{MgAl}_2\text{O}_4$  spinel was investigated using different methods. Differential thermal analysis and thermal gravimetry showed that mechanical activation reduced the spinel formation temperature by around 200 °C, and the corresponding activation energy by about 25%. In addition, characteristic temperatures for evaporation of physisorbed water and decomposition of  $\text{Mg}(\text{OH})_2$  shifted to lower values, and peaks were more pronounced. Raman spectra were used to characterize the degree of inversion as a function of the sintering temperature for all of the sintered specimens, indicating that the breaking point for ordering of the crystal structure was around 1500 °C for non-activated samples, and 1400 °C for activated samples.

**Keywords** Mechanical activation · DTA · Raman spectroscopy · Sintering kinetics · Spinel

## Introduction

Spinel ( $\text{MgAl}_2\text{O}_4$ ) is the only compound in the MgO– $\text{Al}_2\text{O}_3$  binary system [1]. It is a material of great interest owing to its high melting point (> 2100 °C), excellent mechanical, thermal, and chemical properties, and low dielectric constant ( $\sim 8$ ) that make it particularly useful in high-temperature applications [2].  $\text{MgAl}_2\text{O}_4$  can be synthesized through direct solid-state reaction [3, 4], ultrasonic treatment [5], gel-casting [6], wet chemical solution

techniques [7, 8], co-precipitation [9], and mechanical activation [10, 11].

Mechanical activation (MA) is a complex physicochemical process, which increases the chemical activity and potential energy of the treated material, causing changes in the specific surface area and internal energy and generally increasing the free energy of the system [12]. During MA, attrition reduces the crystallite size of the material, which can lead to deformation or changes in the crystal structure, accompanied by generation of defects [13–16]. The influence of the mechanical forces on the material during grinding leads to elastic and plastic deformation, which changes the physicochemical properties of the material [17]. The reactivity of solid materials increases as a result of the structural changes due to generation of point defects (vacancies, interstitial atoms, and impurity atoms), line defects (atom aggregations on the crystal surface), volume defects (pores and impurities), and electronic defects (electrons and holes) [18, 19]. These changes indicate that the mechanical energy was transformed into crystal lattice defects, leading to fragmentation, a decrease in the particle size, and changes in the surface area and the physicochemical properties of crushed material. MA is commonly used as a pre-sintering process

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to improve the reactivity of the system, lower the temperature, and time required for densification or amorphizing the system [20–22].

Spinel exhibits varying degrees of inversion, or disorder among occupancy of A and B sites by the A and B cations, as presented in Fig. 1. The general formula of spinel type of compounds is  $AB_2O_4$ , where A is divalent and B is trivalent. For normal spinels, the A cations occupy 8 of the 64 tetrahedral sites and B cation occupy half of the octahedral sites [23, 24]. With increased temperature or pressure, exchange occurs between Mg and Al cations, leading to the formation of a partially inverted spinel. Inversion usually occurs in the temperature range of 800–1000 °C [25].

Raman spectroscopy can be used to examine the degree of inversion in spinel compounds. To the best of our knowledge, no Raman studies have been reported for spinel specimens sintered above 1400 °C, or for the influence of MA on inversion investigated by characterizing Raman modes. The aim of this study is to determine the influence of the mechanical activation on the microstructure and spinel formation kinetics, which is examined in detail by DTA–TG analysis, as well as the influence of MA on the site occupancy in the  $MgAl_2O_4$  spinel, followed by Raman spectroscopy.

## Experimental

Initial powders were a mixture of high-purity MgO and  $\alpha$ - $Al_2O_3$  (all 99.9% purity Sigma-Aldrich, p.a.), in a 1:1 molar ratio to produce stoichiometric  $MgAl_2O_4$ . The powders were mixed by ball milling to homogenize them without significant particle size reduction. The samples underwent mechanical activation for 60 min in a high-energy planetary ball mill (Planetary Ball Mill Retsch PM 100), in air, using Y-stabilized  $ZrO_2$  vials and balls (5 mm in diameter). The ball-to-powder mass ratio was 40:1 with a rotation speed of 400 rpm. Powders were sieved after

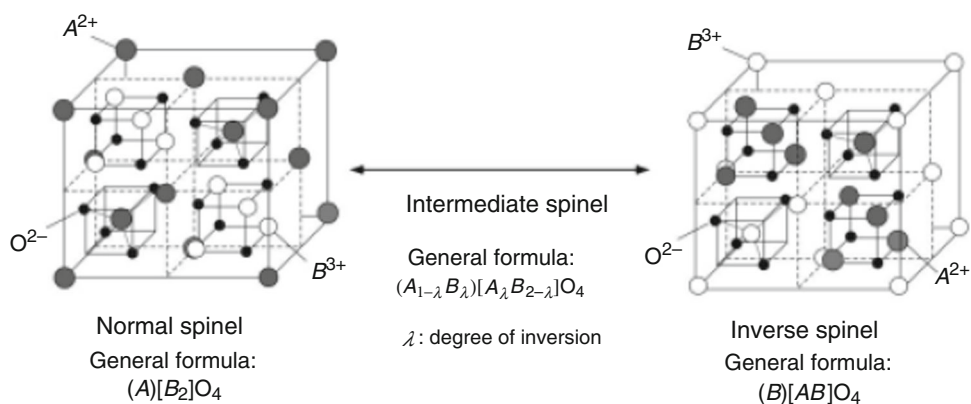
milling. The resulting powders were labeled based on the activation time as AM-0 and AM-60. The binder-free powders were compacted at 300 MPa using a uniaxial double action pressing process with an 8 mm diameter tool (hydraulic press RING, P-14, VEB THURINGER). Compacts were placed in an  $Al_2O_3$  boat and heated in a tube furnace (Lenton Thermal Design Typ 1600). Conventional sintering was performed in air, at temperatures from 1200 to 1600 °C, with heating rates of 10 °C  $min^{-1}$  and 2 h dwell time (isothermal regime on the maximum achieved sintering temperatures). The bulk densities were calculated–measured mass, diameter, and thickness of the sintered specimens. Specimens were labeled according to the sintering temperature, where AM-60-1200 represents the sample mechanically activated for 60 min and sintered at 1200 °C, etc. The theoretical density (TD) of  $MgAl_2O_4$  was assumed to be 3.60  $g\ cm^{-3}$  based on previous reports [23].

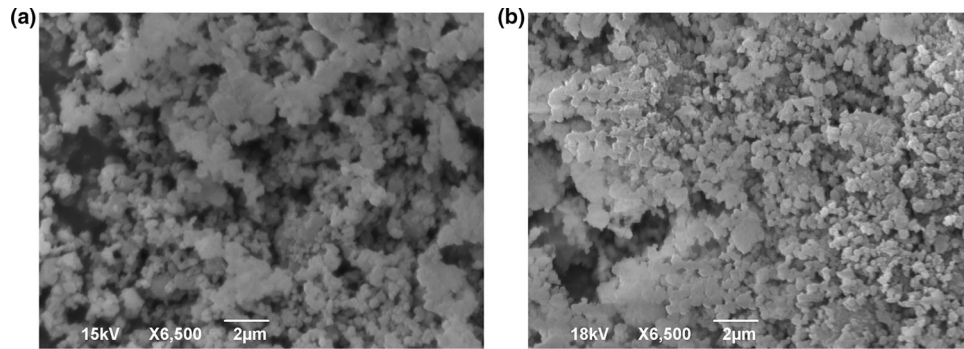
Thermal behavior of powders was determined by simultaneous thermal gravimetry and differential thermal analysis (TG–DTA) (SETSYS, SETARAM Instrumentation, Caluire, France) from 25 to 1500 °C under the air flow of 20  $mL\ min^{-1}$ , in an  $Al_2O_3$  pan, at heating rates of 10, 20, and 30 °C  $min^{-1}$ . Peak deconvolution and kinetic analyses were performed using ThermV v0.2 software package [26]. The degree of conversion ( $\alpha$ ) was calculated for each peak as the ratio of the partial peak area at a given temperature to the area of the entire peak.

The morphology of the powders and sintered specimens was analyzed by the scanning electron microscopy (SEM) (JEOL JSM-6390 LV). Prior to SEM observations, the powders and crushed sintered samples were coated with Au to minimize charging.

The XRD patterns for pulverized sintered specimens were collected on an Ital Structure APD 2000 X-ray powder diffractometer using  $CuK\alpha$  radiation ( $\lambda = 1.5418\ \text{\AA}$ ) in a range  $2\theta = (20^\circ - 80^\circ)$  with a step width of 0.02° and a constant counting time of 1 s per step.

**Fig. 1** Scheme of normal and inverse spinel crystal structure



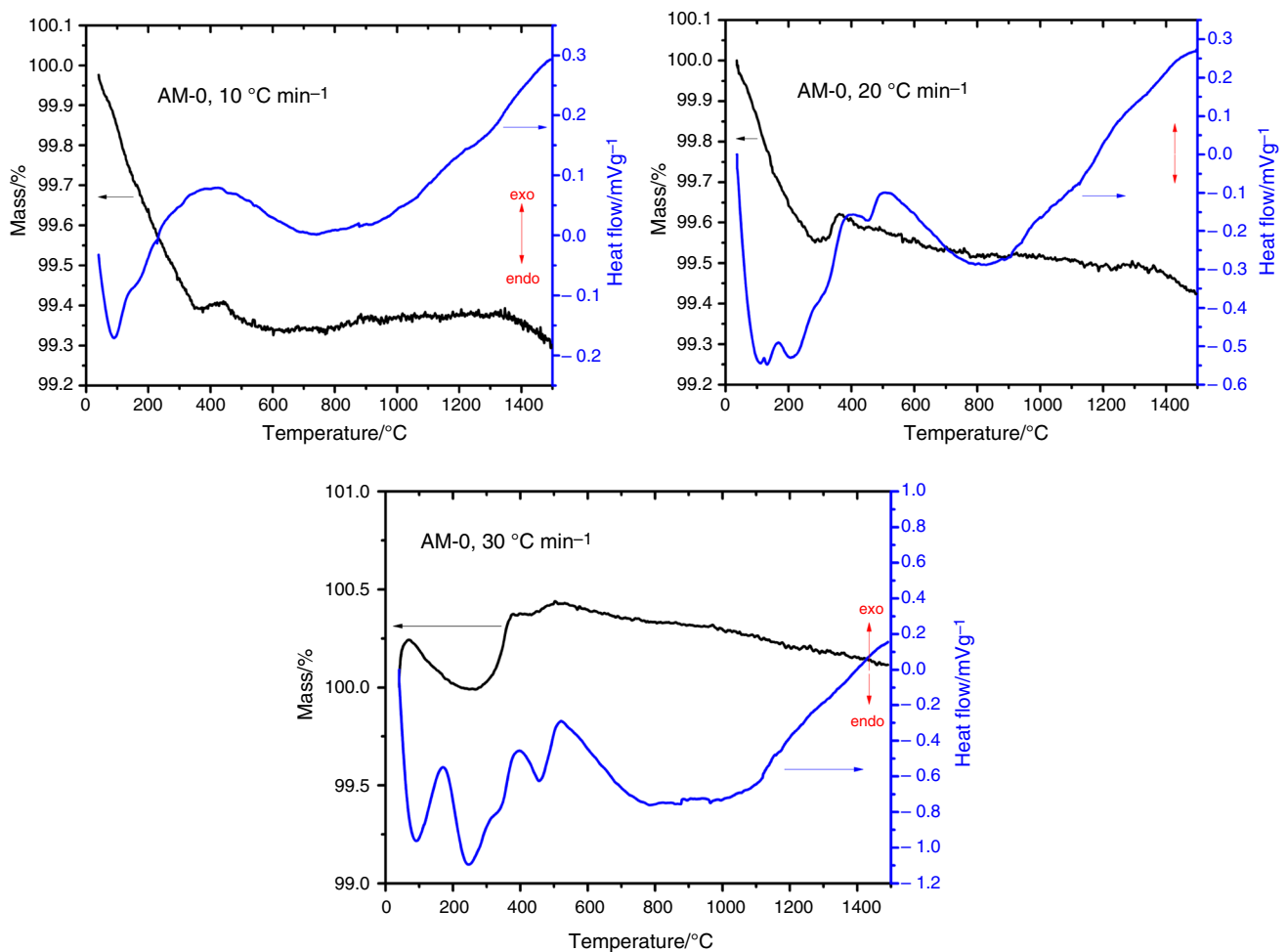


**Fig. 2** SEM micrographs of: **a** non-activated and **b** 60 min activated powder

Raman spectra were recorded in the  $200\text{--}900\text{ cm}^{-1}$  range using a XploRA Raman spectrometer from Horiba Jobin–Yvon, with a 532 nm laser at a maximum output power of 20–25 mW. To prevent damage by the laser, power was reduced using a 10% filter. All measurements were realized using a spectrometer equipped with a 2400

lines  $\text{mm}^{-1}$  grating, with 10 s/5 cycles acquisition time. A microscope objective ( $50\times$ , long working distance) was used for laser focusing.

An Agilent E5061A network analyzer was used to measure the relative dielectric permittivity (dielectric constant) and the loss tangent of the sintered specimens in



**Fig. 3** DTA–TG results for non-activated samples with different heating rates

the frequency range between 10 MHz and 3 GHz, in a coaxial test chamber. The reflection coefficient of the chamber was measured by the analyzer, and electromagnetic models were used to extract the relative complex permittivity of the specimens.

## Results and discussion

Scanning electron micrographs of the starting powders are presented in Fig. 2. The non-activated powder consisted of two different types of particles: (1) smaller primary particles approximately 300 nm in diameter that was present in agglomerates around 1  $\mu\text{m}$  in size; and (2) larger polygonal particles ranging in size from about 1.5 to 2.5  $\mu\text{m}$ .

The influence of MA on powder morphology is evident in the powder activated for 60 min, which appeared to be more homogeneous with an obvious reduction in agglomerate and particle size. The change in morphology indicated that smaller particles formed as MgO agglomerates were comminuted. Larger alumina particles were also

broken down into particles that were 1  $\mu\text{m}$  or smaller in diameter.

The DTA curves of non-activated powders had some very weak peaks shown in Fig. 3. In contrast, the activated samples had more pronounced peaks as shown in Fig. 4. In both non-activated and activated powders, an increase in heating rate led to more pronounced endothermic peaks. All curves possessed an endothermic peak at around 100  $^{\circ}\text{C}$ , which was attributed to loss of adsorbed water. In the temperature range of 200–350  $^{\circ}\text{C}$ , several processes occurred, such as loss of chemically bound water or related compounds [27, 28]. Given that both the mechanical activation and thermal experiments were performed in the air, it is likely that carbon dioxide was physisorbed or chemisorbed in the activated powders, leading to additional desorption processes at higher temperatures.

Significantly higher mass loss was observed for mechanically activated samples. The higher mass losses further reinforce the assignments of mass loss to loss of water and/or  $\text{CO}_2$ , with mass losses of 0.4–0.6 mass% in non-activated and 3.5–4 mass% in activated samples.

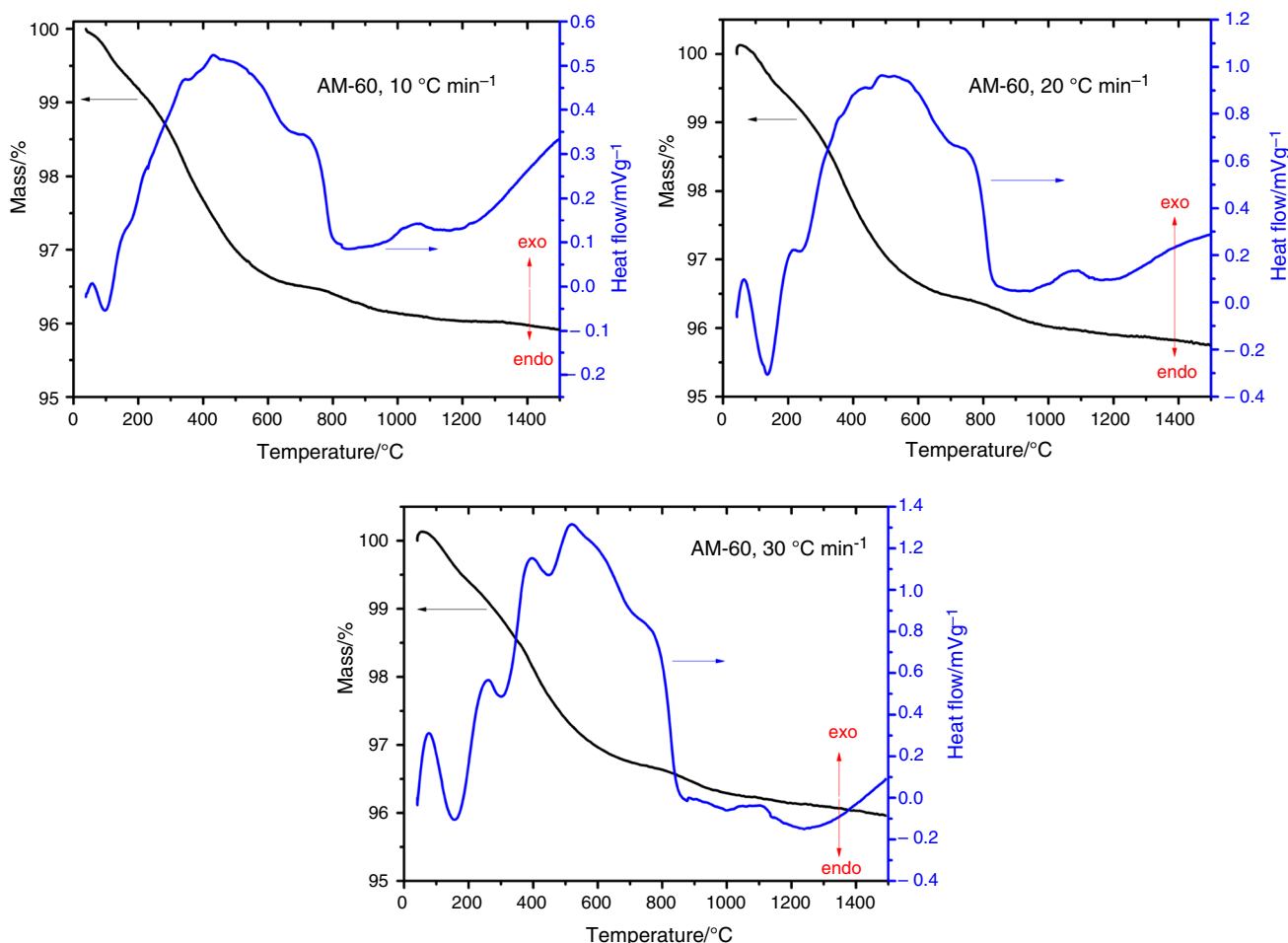
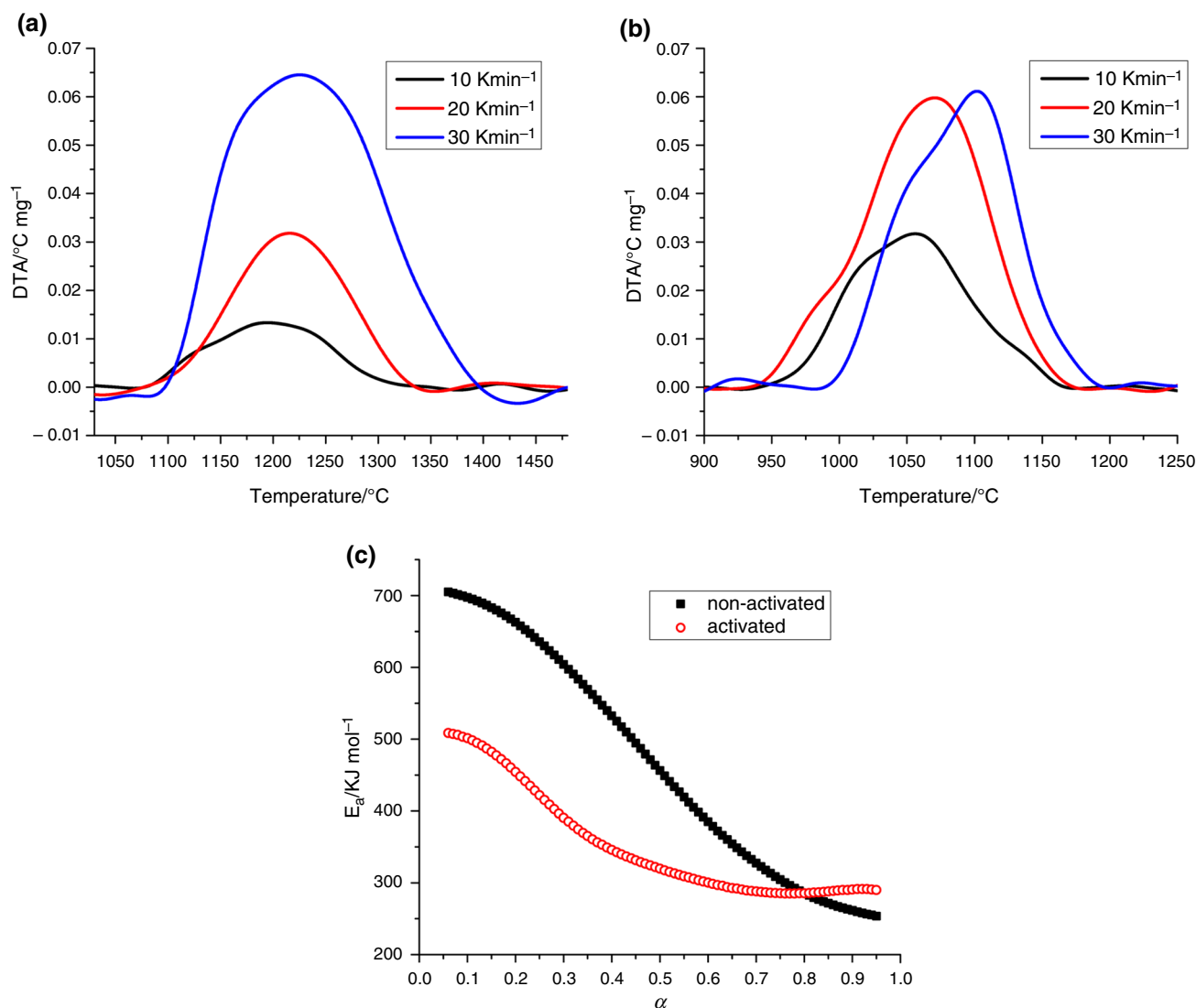


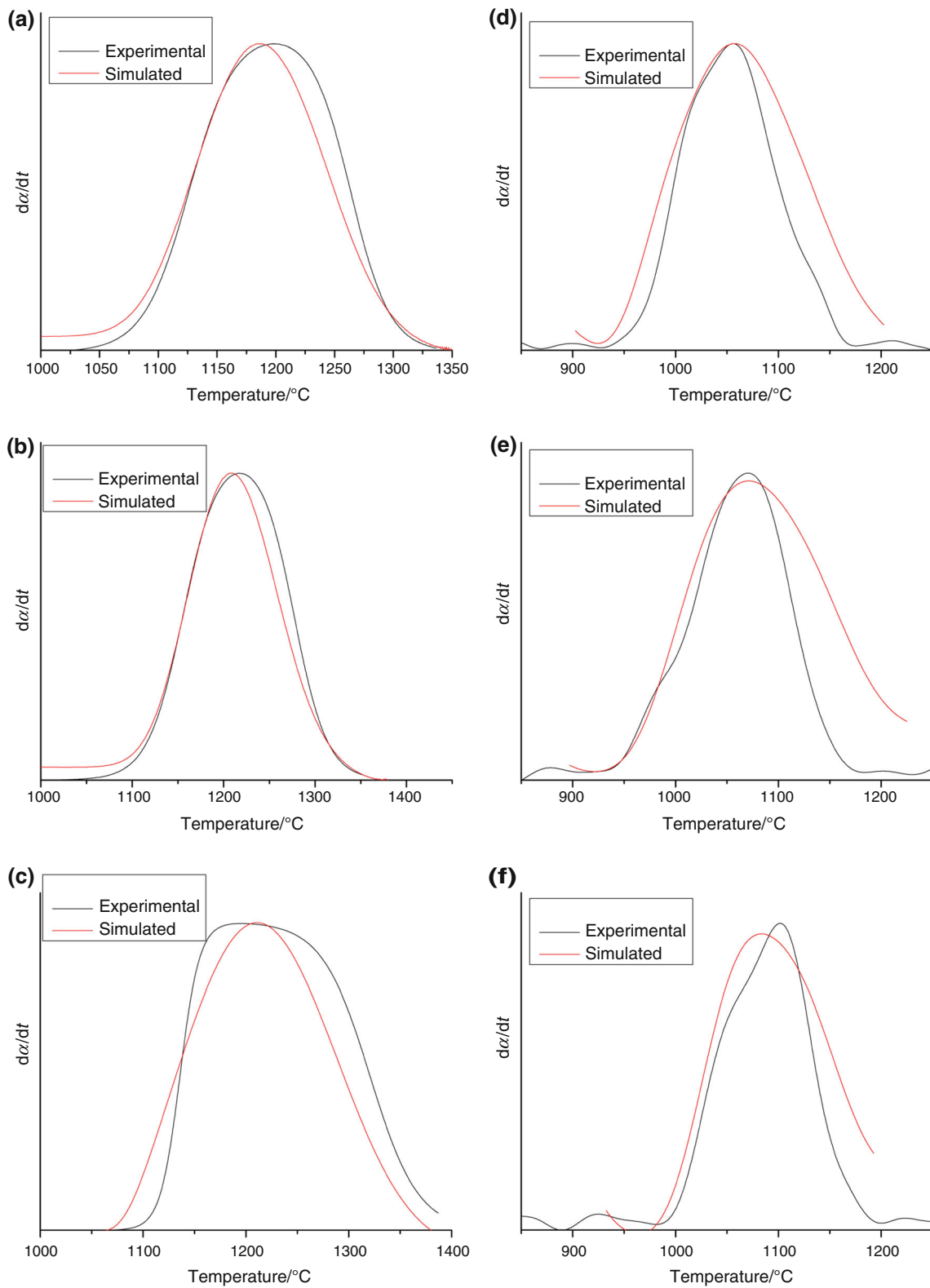
Fig. 4 DTA–TG results for activated samples with different heating rates

Around 455 °C, an endothermic peak was observed for all samples, which can be attributed to dehydration of magnesium hydroxide and decomposition of magnesium carbonate, [29, 30]. Unlike other peaks, the peak due to dehydration of magnesium hydroxide and carbonate decomposition was more pronounced in non-activated samples, which is consistent with the fact that the mechanical activation in air would partially disrupt the existing surface layer due to the increase in surface area while also introducing a significant amount of additional carbon dioxide into the powder mixture prior to thermal analysis. Above 500 °C, no additional mass changes were observed. At temperatures above 500 °C, a relatively small endothermic peak was observed around 700 °C for mechanically activated samples.

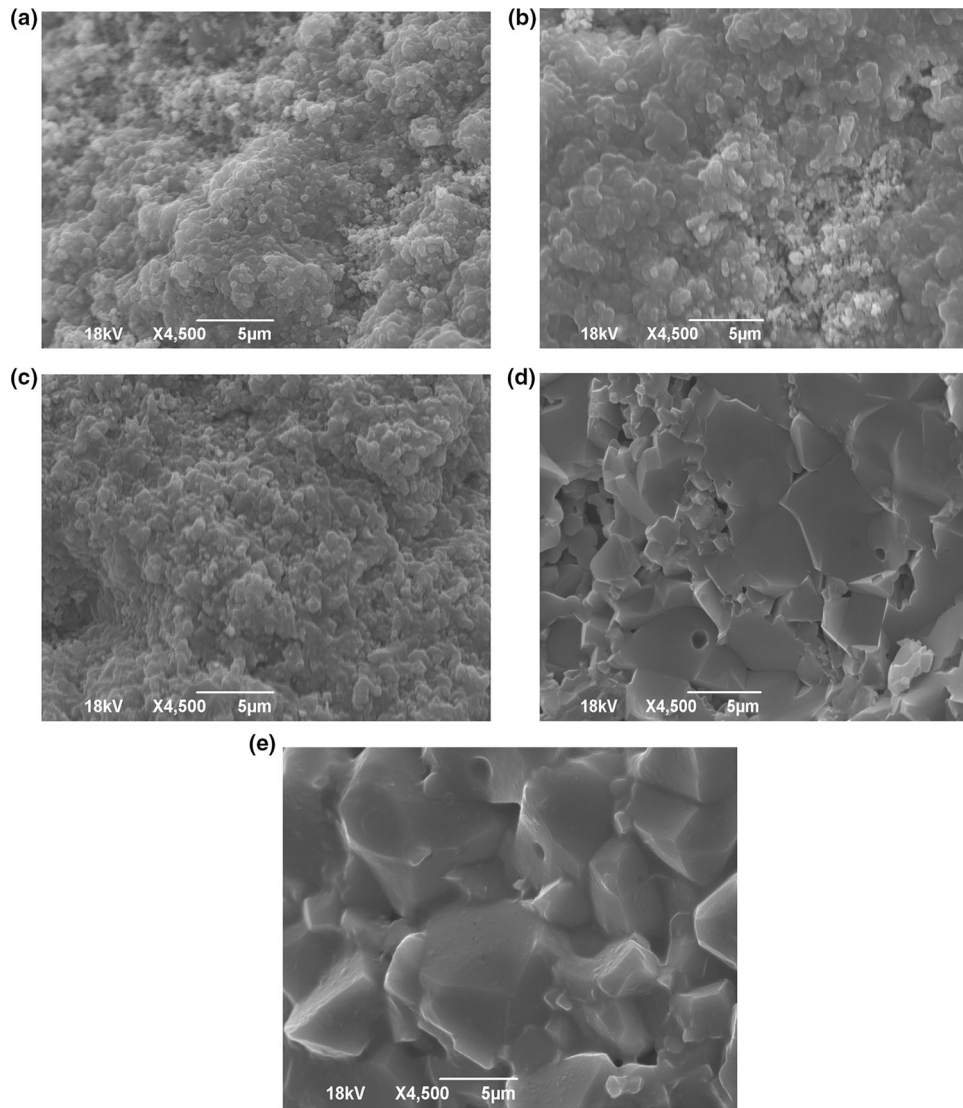
Mechanical activation led to more rapid spinel formation at lower temperatures. An exothermic peak was observed for all samples in the temperature range of 950–1400 °C, which corresponded to spinel formation [9] (Fig. 5). The lower temperature of the exothermic peak in the activated samples indicated significantly greater reactivity of the powder activated for 60 min. Furthermore, the reaction required less energy to reach completion based on the overall activation energies ( $E_a$ ), calculated using Kissinger method [31]. The  $E_a$  values were  $580 \pm 10 \text{ kJ mol}^{-1}$  for the non-activated powder and  $420 \pm 15 \text{ kJ mol}^{-1}$  for the activated sample. The non-activated powder had a similar  $E_a$  to a previously reported values of around  $550 \text{ kJ mol}^{-1}$  [32]. The corresponding values of the pre-exponential factor ( $A$ ) were also lower for the activated powders with  $\ln A$  values of  $31.0 \pm 0.5$  for the



**Fig. 5** Spinel formation peaks from DTA in: **a** non-activated and **b** activated powders; **c** effective values of  $E_a$  (isoconversional Ortega method) for formation of spinel



**Fig. 6** Comparison of experimental and simulated curves for non-activated (a–c) and activated (d–f) samples at different heating rates with presumed model D2



**Fig. 7** SEM micrographs of fracture surfaces of specimens: **a** AM-0-1200, **b** AM-0-1300, **c** AM-0-1400, **d** AM-0-1500, and **e** AM-0-1600

non-activated powder and  $22.0 \pm 0.8$  for the activated powder. The lower value of the activation energy for spinel formation from mechanically activated powders is consistent with the reduction in observed spinel formation temperature from 1100–1400 °C for the non-activated powder to 950–1150 °C for the activated powder.

The reduction in formation temperature can be attributed to the increase in the powder surface area, which increases the number of potential nucleation sites for spinel formation in the mechanically activated precursor powders and increases the concentration of defects caused by the mechanical activation [13]. The peaks in mechanically activated powders were also considerably narrower, indicating faster reaction for activated powders. Based on this analysis, mechanical activation reduces the spinel formation temperature and increases the reaction rate by reducing

the activation energy required for reaction. Figure 5 also shows the effective apparent values of the activation energy for both non-activated and activated samples, obtained using the isoconversional Ortega method [33] for the exothermic spinel formation peak. Calculated values of  $E_a$  are considerably lower for mechanically activated samples, and the shape of both curves, with a downward slope, indicates a process complicated by diffusion [34], consistent with mass transport during formation of spinel in the solid state.

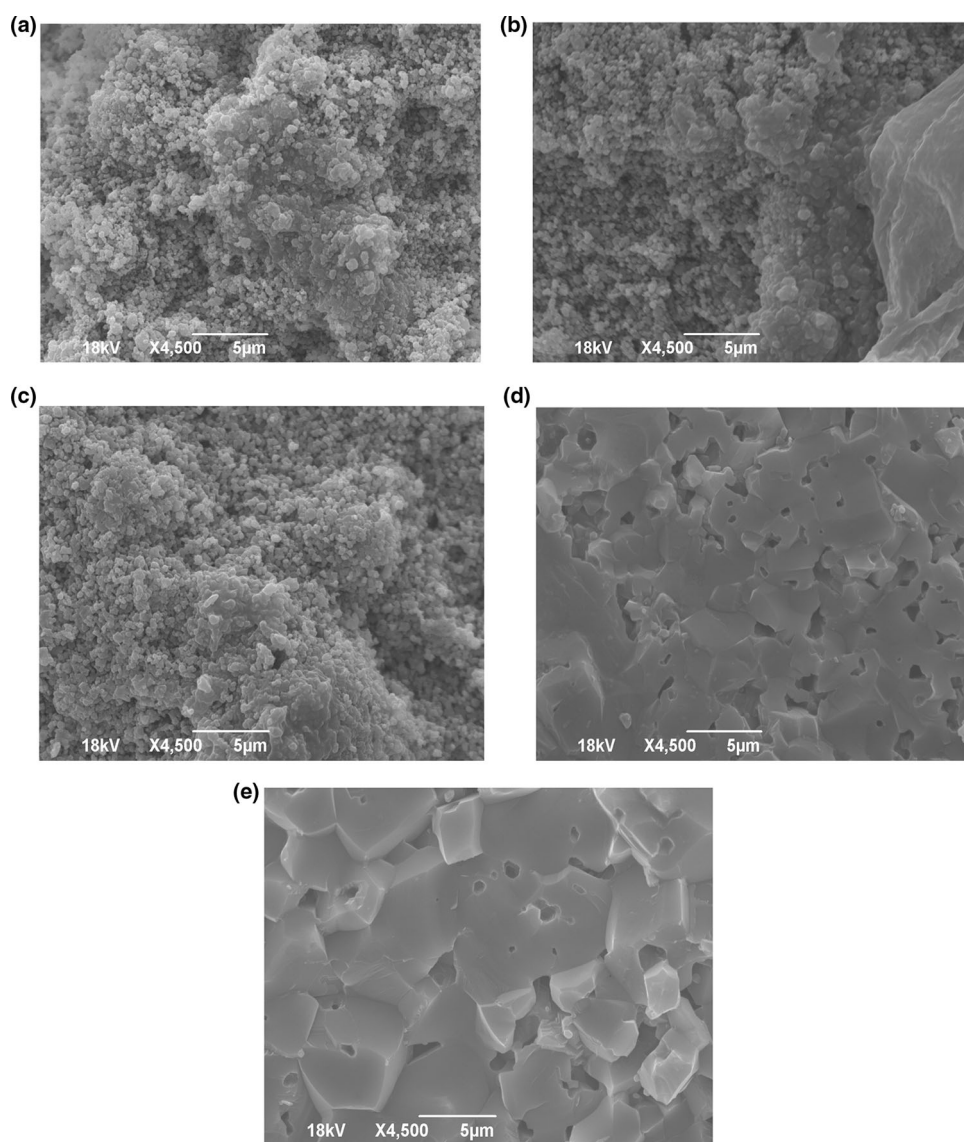
Figure 6 shows comparison of simulated curves calculated using kinetic parameters obtained from Kissinger method above and assuming D2: 2-D diffusion reaction model [35]. These show that non-activated samples exhibit, in general, higher agreement with D2 model, while mechanically activated samples only show good agreement

**Table 1** Final bulk densities ( $\rho$ ) and relative permittivity for sintered samples

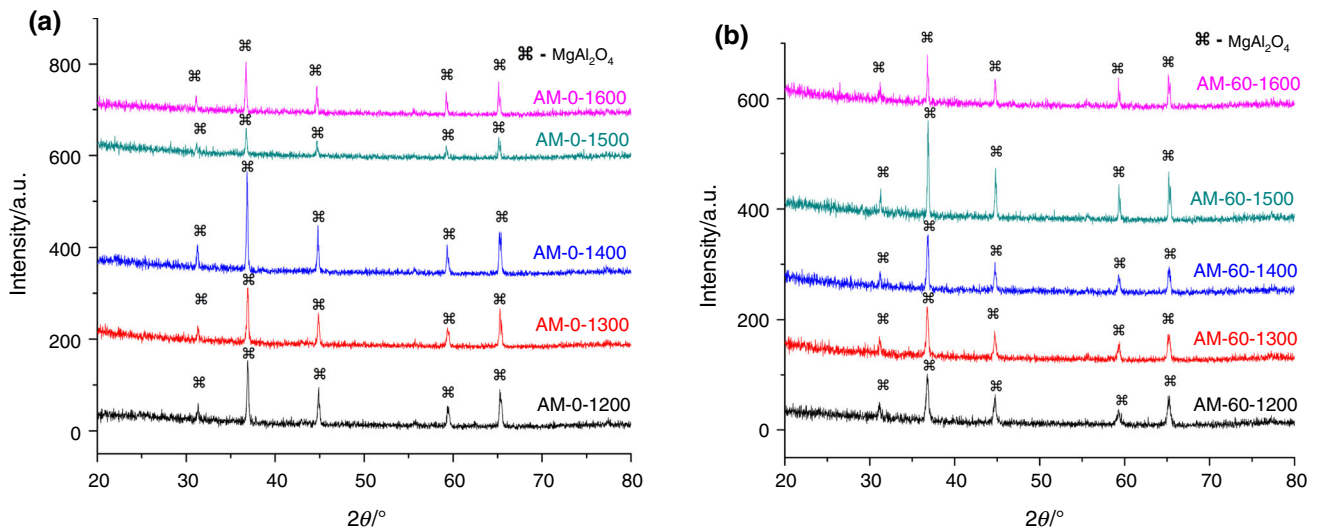
Sample	$\rho/\text{g cm}^{-3}$	$\epsilon_r$
AM-0-1200	1.75	2.91
AM-60-1200	1.83	3.28
AM-0-1300	1.61	3.21
AM-60-1300	1.90	3.53
AM-0-1400	2.08	3.49
AM-60-1400	2.22	4.04
AM-0-1500	2.86	4.41
AM-60-1500	2.71	4.69
AM-0-1600	3.26	6.15
AM-60-1600	3.21	5.65

in the initial stage of the reaction, which can be attributed to the increased complexity caused by the mechanical activation. General agreement with 2-D diffusion reaction model can be expected for a solid-state reaction in the powder mixture.

Scanning electron micrographs of fracture surfaces of the sintered specimens produced from the non-activated powders (AM-0 series) are presented in Fig. 7. The non-activated specimen sintered at 1200 °C for 2 h consisted of particles approx. 500 nm in size with necks that formed during sintering. Specimen AM-0-1300 showed a higher degree of sintering. In addition to the non-uniform grain size, cracks were present, which were presumed to form

**Fig. 8** SEM micrographs of fracture surfaces of sintered samples: **a** AM-60-1200, **b** AM-60-1300, **c** AM-60-1400, **d** AM-60-1500, and **e** AM-60-1600





**Fig. 9** XRD patterns of: **a** non-activated powder (AM-0) and **b** powder activated for 60 min (AM-60), after heating to various temperatures for 2 h in air [10]

around regions that corresponded to agglomerates in the initial powder compact that had higher density after sintering at this temperature. After sintering at 1400 °C, the observed microstructure was very similar to the samples sintered at lower temperatures, with breakage between grains, irregular pores, and agglomerates visible, indicating that the grain growth had not yet started and that this specimen remained in the intermediate stage of sintering.

Spherical pores and breakage through grains observed for AM-0-1500 indicated that this specimen had entered the final sintering stage. Some breakage between smaller grains was observed, confirming that those grains were not fully developed, with non-uniform grain growth observed, as well. When the sintering temperature was increased to 1600 °C, all of the grains were polygonal with small, spherical, and closed pores. Based on its appearance, AM-0-1600 had a high relative density and appeared to be completely sintered, in agreement with measured densities (see Table 1).

Figure 8a shows that AM-60-1200 consisted of powder particles less than 500 nm in size, with fully open porosity and contact necks formed between all of the particles. The AM-60-1300 specimen had some regions that appeared to be sintered to a higher relative density (see the right part of Fig. 8b), with the other portion of the sample indicating that the specimen consisted of particles which had started to form necks. The presence of the open porosity and non-uniform microstructural regions indicated that this specimen was still in the initial sintering stage. The main characteristics for AM-60-1400 were breakage through grains and uniform grain size with open porosity, where the pores were becoming more spheroidal and the dominant fracture mode was through grain. At this temperature,

microstructures were almost completely compact. Non-uniform grain growth was observed in AM-60-1500 with uneven pores. Compared to lower sintering temperatures, the degree of porosity was significantly lower and additional polygonal grains had formed. Most pores were coalescing into closed pores, indicative of final stage sintering, which was observed in AM-60-1600.

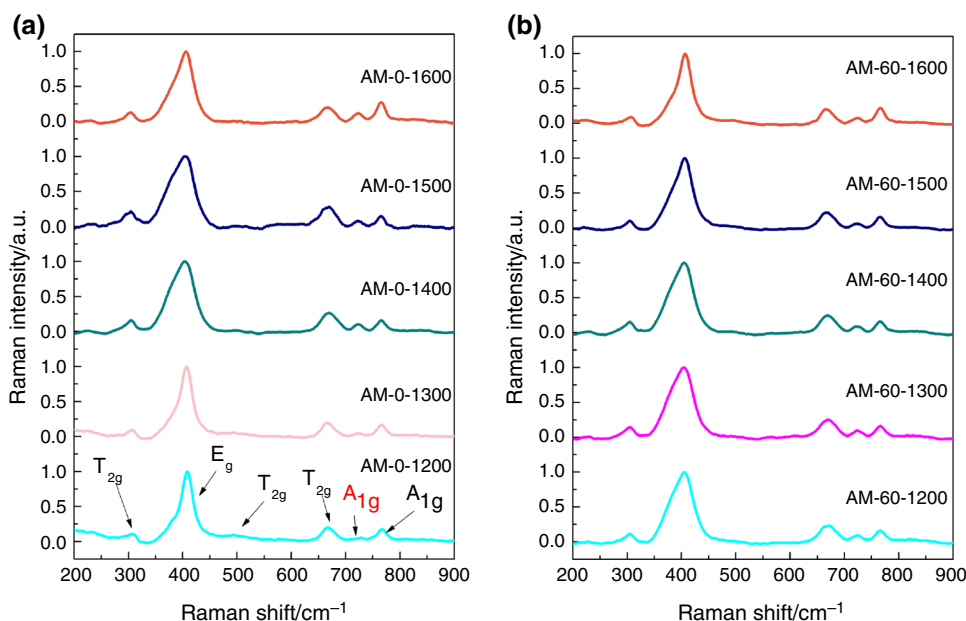
The XRD patterns of sintered specimens are presented in Fig. 9. All reflections were identified using the corresponding JCPDS card 33–0853 for MgAl<sub>2</sub>O<sub>4</sub>. All peaks were sharp, indicating that the MgO and Al<sub>2</sub>O<sub>3</sub> powders reacted to form the spinel phase of MgAl<sub>2</sub>O<sub>4</sub>.

The relative permittivity ( $\epsilon_r$ ) of the measured samples is shown in Table 1 along with the bulk densities. For all specimens, the relative permittivity was nearly independent of frequency between 10 MHz and 3 GHz. The measured loss tangent was below the resolution of the measurement method ( $\leq 0.005$ ), indicating very low dielectric losses.

The dependence of the relative permittivity on the sintering temperature followed the same trend as that of the bulk density [36]. The density increased with the sintering temperature, indicating that higher sintering temperatures led to lower porosity and more compact structures, which is consistent with the observed changes in the microstructures (see Figs. 7 and 8).

This suggests that the higher density and more homogeneous microstructures were responsible for the higher dielectric permittivity obtained for increased sintering temperatures. The permittivity increased more than 100%, from as low as  $\sim 2.9$  for AM-0-1200, to over 6 for AM-0-1600. Mechanically activated samples exhibit consistently higher values of the bulk density and permittivity at sintering temperatures below 1600 °C, due to the smaller

**Fig. 10** Raman spectra of: **a** non-activated and **b** activated samples sintered in the range 1200–1600 °C



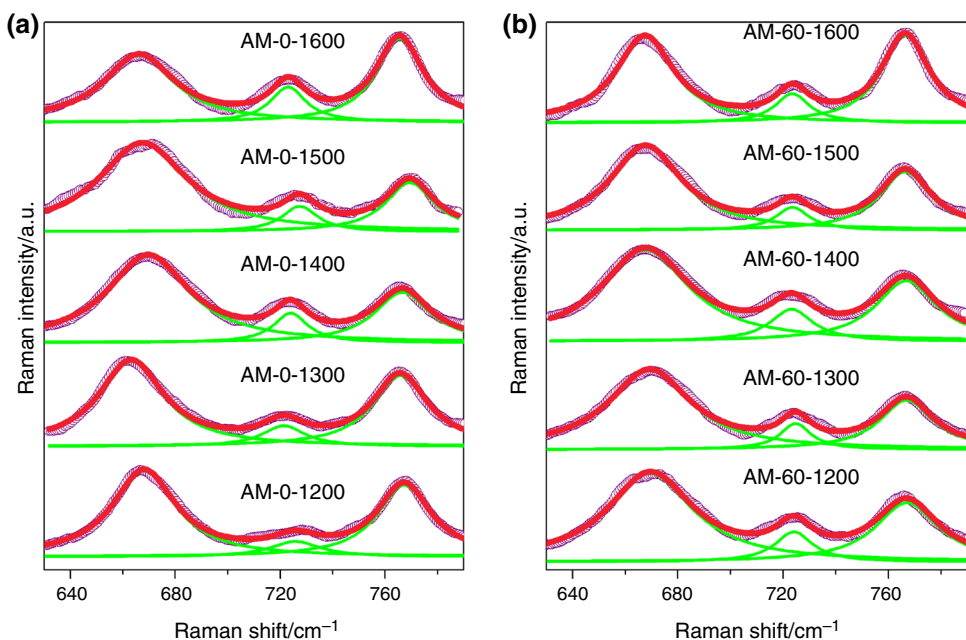
particle size and improved sintering caused by the mechanical activation [10].

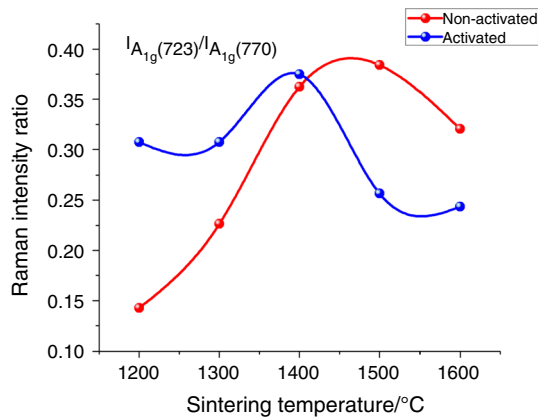
Raman spectra of non-activated and mechanically activated samples, sintered in the range 1200–1600 °C, are presented in Fig. 10.  $\text{MgAl}_2\text{O}_4$  belongs to the space group  $Fd\bar{3}m$  and exhibits five Raman active modes ( $A_{1g} + E_g + 3T_{2g}$ ) [37, 38]. All five Raman active modes were observed, and their positions and intensity ratios were in good agreement with literature data. In normal spinel, only two sharp and well-defined peaks were observed above  $600\text{ cm}^{-1}$ , while for the inverse spinel, an additional  $A_{1g}$  peak appears at about  $724\text{ cm}^{-1}$  [39, 40]. The presence of

this additional  $A_{1g}$  peak is observed in all Raman spectra shown in Fig. 10, indicating the degree of disorder. The lowest intensity of this peak is detected for AM-0-1200, and with increasing sintering temperature, the intensity of the peak increased, along with broadening of all observed peaks, suggesting an increase in the degree of disorder.

The effects of sintering temperature and mechanical activation on disorder were investigated in more detail by deconvoluting the Raman spectra. Peaks in the range  $630\text{--}800\text{ cm}^{-1}$  were fit to individual Lorentzian peaks as shown in Fig. 11. A previous study has shown that the mode at  $\sim 723\text{ cm}^{-1}$  has the same symmetry as the mode

**Fig. 11** Deconvolution of Raman spectra of: **a** non-activated and sintered samples and **b** activated and sintered samples (green lines—separated Lorentzian peaks, red line—sum of Lorentzian peaks, blue circles—measured data). (Color figure online)





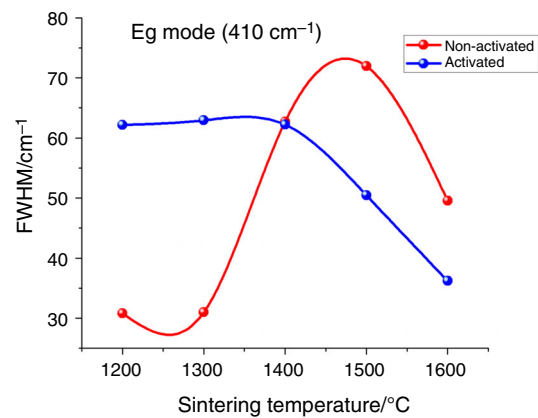
**Fig. 12** Intensity ratio of Lorentzian peaks at  $\sim 723$  and  $\sim 770 \text{ cm}^{-1}$  as a function of sintering temperature for non-activated and activated powders

at  $\sim 770 \text{ cm}^{-1}$  [24]. The peak at  $\sim 723 \text{ cm}^{-1}$  has been identified as a breathing mode of  $\text{AlO}_4$  tetrahedral, which is connected to the presence of cationic disorder.

In contrast, the peak at  $\sim 770 \text{ cm}^{-1}$  has been identified as symmetric stretching of  $\text{Mg-O}$  bonds in  $\text{MgO}_4$  tetrahedra, which is correlated to an ordered structure. Hence, the intensity ratio of these separated Lorentzian peaks can be used as a measure of disorder in  $\text{MgAl}_2\text{O}_4$ . The intensity ratios of peaks at  $723$  and  $770 \text{ cm}^{-1}$ , for non-activated and activated samples vs. sintering temperature, are presented in Fig. 12.

The level of disorder initially increased with increasing sintering temperature. As shown in Fig. 12, the level of disorder increased up to  $1500 \text{ }^\circ\text{C}$  for non-activated powders and  $1400 \text{ }^\circ\text{C}$  for activated samples. The initial increase in disorder with increasing sintering temperature is consistent with previous reports while the decrease at higher temperatures is presumably due to annihilation of defects at higher temperatures. Comparing the non-activated and activated samples shows that mechanical activation leads to an increase in the degree of the exchange between  $\text{Mg}$  and  $\text{Al}$  cations, which may be due to the introduction of defects during the milling process.

In addition to the peak intensity ratios, disorder in spinel structure can be observed through changes in symmetry and width of  $E_g$  mode at  $\sim 410 \text{ cm}^{-1}$ , where the width of this mode increased due to an increase in inverse spinel content with increasing temperature [24, 37]. According to available literature data, all previous studies involving Raman measurements for  $\text{MgAl}_2\text{O}_4$  spinel were performed for materials heat up to only  $1400 \text{ }^\circ\text{C}$  [24, 37, 38]. The present study extends the investigation of the order-disorder ratio to samples sintered up to  $1600 \text{ }^\circ\text{C}$ . Changes in width of  $E_g$  mode were fitted by a Lorentzian function, and the obtained results are presented in Fig. 13. Changes in the full width at the half maximum (FWHM) of  $E_g$  peak



**Fig. 13** The FWHM values of the  $410 \text{ cm}^{-1}$  mode as a function of the sintering temperatures for non-activated and mechanically activated samples

followed same trend as the changes in the intensity ratio of Lorentzian peaks at  $\sim 723$  and  $\sim 770 \text{ cm}^{-1}$ . For non-activated samples, the breaking point for ordering of the crystal structure was around  $1500 \text{ }^\circ\text{C}$ , while this point shifted to  $1400 \text{ }^\circ\text{C}$  for activated samples, indicating that mechanical activation lowers the temperature of the ordering of the crystal lattice by about  $100 \text{ }^\circ\text{C}$ .

## Conclusions

The influence of mechanical activation on microstructure, crystallization kinetics, and cation ordering in the  $\text{MgAl}_2\text{O}_4$  spinel was investigated. The main conclusions are:

- 60 min of mechanical activation led to mechanochemical reaction within the initial powder; activation produced powders that appeared to be homogeneous with a reduction in agglomerate and particle size, compared to the non-activated powders.
- DTA indicated several processes took place during heating: loss of adsorbed water, decomposition of  $\text{Mg}(\text{OH})_2$ , and decarbonization of  $\text{MgO}$ . In addition, an exothermic peak corresponding to the spinel formation was observed. This peak shifting from  $1100\text{--}1400 \text{ }^\circ\text{C}$  for non-activated powders to  $950\text{--}1150 \text{ }^\circ\text{C}$  after activation, with a corresponding reduction in value of  $E_a$  from  $580$  to  $420 \text{ kJ mol}^{-1}$ .
- Analysis of microstructures showed that AM-0-1600 and AM-60-1600 had no open porosity, indicating that the final stage sintering was reached. As density increased, the pores became more regular in shape. The increased density also led to increases in the dielectric permittivity, from the lowest values of less than 3 after sintering at  $1200 \text{ }^\circ\text{C}$  to values of more than 6 after sintering at  $1600 \text{ }^\circ\text{C}$ . Furthermore, one-phase system after sintering is obtained for all samples.

4. Cation inversion was observed in all of sintered samples based additional Raman peak at  $724\text{ cm}^{-1}$ . An increase in inversion was observed with increasing sintering temperature, and the degree of inversion was higher in mechanically activated samples. Detailed analysis of Raman spectra indicated the breaking point for ordering of crystal structure to be around  $1500\text{ }^{\circ}\text{C}$  for non-activated samples, while that point for activated samples is shifted to  $1400\text{ }^{\circ}\text{C}$ .
5. Finally, mechanical activation, as a preparation process, had a strong influence on all hierarchical levels within the powders and sintered samples: It affected the chemical reaction, lowered the temperature of the spinel formation by about  $200\text{ }^{\circ}\text{C}$ , and lowered the temperature of arrangement of the crystal lattice by about  $100\text{ }^{\circ}\text{C}$ .

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